

MATHEMATICAL TRIPOS      Part III

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Wednesday, 8 June, 2022    9:00 am to 12:00 pm

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PAPER 332

FLUID DYNAMICS OF THE SOLID EARTH

Before you begin please read these instructions carefully

Candidates have THREE HOURS to complete the written examination.

Attempt all **THREE** questions.  
There are **THREE** questions in total.  
The questions carry equal weight.

**STATIONERY REQUIREMENTS**

Cover sheet  
Treasury tag  
Script paper  
Rough paper

**SPECIAL REQUIREMENTS**

None

<p>You may not start to read the questions printed on the subsequent pages until instructed to do so by the Invigilator.</p>
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## 1

- (a) Rain falls on a two-dimensional, unconfined aquifer at rainfall rate  $R$ , which results in a groundwater table of thickness  $h(x, t)$  that feeds a river at  $x = 0$  and extends to the drainage divide at  $x = L$ , across which there is no groundwater flow.

Starting from the equations for flow of water of viscosity  $\mu$  and density  $\rho$  in a porous medium with porosity  $1 - \phi$  and permeability  $k$  derive the leading-order equations for the transient response of the groundwater table in the limit  $h \ll L$ ,

$$(1 - \phi) \frac{\partial h}{\partial t} = \frac{k \rho g}{\mu} \frac{\partial}{\partial x} \left( h \frac{\partial h}{\partial x} \right) + R, \quad (1)$$

where  $g$  is the gravitational acceleration.

If the height of the groundwater table at the river  $h(0, t) = 0$  derive the response of the groundwater table, providing expressions for the flux into the river  $q(0, t)$  and the asymptotic form of the groundwater table near the river ( $x \ll L$ ) in three cases:

- (i) the transient groundwater response to rainfall  $R > 0$  for  $t > 0$  starting from initial condition  $h(x, 0) = 0$ ;
- (ii) the steady-state groundwater profile when  $R$  is constant, as  $t \rightarrow \infty$ ;
- (iii) the late-time transient drawdown of the aquifer when  $R = 0$ .

[You do not need to solve intractable nonlinear equations but should set out clearly what equations need to be solved with what boundary conditions.]

- (b) Now consider the influence of tidal forcing on the flow of the aquifer. Approximate the tidal forcing as a small variation in local gravity,

$$g = g_0(1 + \epsilon e^{i\omega t}),$$

where  $\epsilon \ll 1$  and  $\omega$  is the tidal frequency. The aquifer behaves as an isotropic, poroelastic medium and you may approximate the effective stress as

$$\sigma_e = E \frac{\phi_0 - \phi}{\phi_0},$$

where  $E$  is Young's modulus and  $\phi_0$  is the undeformed solid fraction. Derive an expression for the solid fraction of the aquifer,

$$\phi = \phi_0 \exp[g'(h - z)/l_c],$$

in terms of the variation of gravity  $g' = g/g_0$  and the compaction length  $l_c$ , which should be expressed in terms of constant physical properties. Show that in the limit  $h \ll l_c$ , the volume of water per unit horizontal distance is

$$V = (1 - \phi_0)h - \phi_0 \frac{g'h^2}{2l_c}.$$

Derive an integral expression for the flux of water into the river in terms of  $V$  and hence, using scaling or otherwise, estimate the magnitude of the variation in the flux relative to its mean.

## 2

A solid grows one-dimensionally into a supercooled melt of initial temperature  $T_\infty < T_m$ , where  $T_m$  is the equilibrium freezing temperature of the melt. The rate of solidification is determined kinetically by

$$V = \mathcal{G}(T_m - T_i),$$

where  $\mathcal{G}$  is a constant and  $T_i$  is the temperature of the solid–melt interface. Show that there is a steady state with  $V = \mathcal{G}\Delta T(1 - \mathcal{S})$ , provided the Stefan number  $\mathcal{S} = L/c_p\Delta T < 1$ , where  $\Delta T = T_m - T_\infty$ ,  $L$  is the latent heat of fusion and  $c_p$  is the specific heat capacity.

Use a linear stability analysis to find a general dispersion relation for the growth rate of perturbations to the interface and thermal field, and show that the interface is marginally stable when

$$\frac{\mathcal{S}}{1 - \mathcal{S}} = \Gamma \frac{\lambda}{\lambda - 1} \alpha^2,$$

where

$$\lambda = \frac{1}{2} \left( 1 + \sqrt{1 + 4\alpha^2} \right).$$

Here,  $\alpha$  is the dimensionless wavenumber, lengths are scaled by  $\kappa/V$ , and  $\Gamma = \gamma\mathcal{G}/\kappa$ , where  $\gamma$  is the constant of proportionality between the interfacial undercooling related to curvature and the curvature itself, and  $\kappa$  is the thermal diffusivity.

Using sketch graphs and an asymptotic analysis, show that the solid is morphologically unstable if  $\mathcal{S} > \Gamma/(1 + \Gamma)$  and that the range of unstable wavenumbers becomes infinite as  $\mathcal{S} \rightarrow 1$ .

**3**

- a) A two-dimensional terrestrial ice sheet, treated as a layer of Newtonian fluid of kinematic viscosity  $\nu$  and thickness  $h(x, t)$  flowing over flat bedrock, is subject to a net accumulation rate

$$\begin{aligned} a &= A \quad \text{if } h > h_s \\ a &= -A \quad \text{if } h < h_s, \end{aligned}$$

where  $x$  is horizontal distance,  $t$  is time,  $A$  is constant, and the elevation of the snow line  $h_s$  is constant.

Use thin-film theory to develop evolution equations for  $h(x, t)$  in the regions  $|x| < x_s$  and  $x_s < |x| < x_N$ , where  $|x| = x_s$  are the horizontal positions of the snow line and  $|x| = x_N$  are the termini of the ice sheet. What boundary/interfacial conditions apply to these equations at the ice divide  $x = 0$ , the termini  $x = x_N$  and the snow line  $x = x_s$ ?

Find the steady shape  $h(x)$  of the ice sheet and use your solution to determine its maximum thickness  $h_0$ , its horizontal extent  $x_N$ , and the horizontal position of the snow line

$$x_s = \left( \frac{g}{6\nu A} \right)^{1/2} h_s^2.$$

Deduce that your analysis is appropriate provided that  $A \ll gh_s^2/\nu$ .

- b) Now consider the case of a marine ice sheet in which the bedrock is a constant distance  $b$  below sea level. Derive the boundary conditions that apply to the ice sheet at the grounding line  $|x| = x_G$ . Assuming that for the marine ice sheet  $A \ll g'h_G^2/\nu$ , determine that the position of the grounding line  $x_G$  is given by

$$x_G = 2x_s - \frac{\sqrt{gg'}}{6\nu A} h_G^3,$$

where  $g' = g(\rho_w - \rho)/\rho_w$ ,  $\rho_w$  is the density of sea water, and  $h_G = b\rho_w/\rho$  is the thickness of the ice sheet at the grounding line. Hence show that the horizontal position of the snow line is now

$$x_s \approx \left( \frac{g}{6\nu A} \right)^{1/2} \left( h_s^4 + \frac{g'}{6\nu A} h_G^6 \right)^{1/2}.$$

What is the maximum thickness of the marine ice sheet?

**END OF PAPER**